Example 2.1 Pad foundation with vertical central load on dense sand Note: this is a persistent design situation; for simplicity, accidental design situations do NOT need to be checked.

Question		Instruction	Answer				
GENERAL							
I	in case we need to clarify your submission*	strictly confidential	Name Pawel Galas Affiliation Department of Geotechnical Engineering, Warsaw University of Life Sciences, Warsaw, Poland Email address galaspawel@o2.pl				
2	How many structures of this kind have you previously designed?	Tick one	□ None ⊠ 1-2 □ 3-6 □ More than 6				
3	Having completed your design to Eurocode 7, how confident are you that the design is sound?	Tick one	□ Very unsure □ Unsure				
4	How did you account for the location of cone tests relative to the foundation?	Tick one	 Did not consider test location Considered nearest test only Considered 'average' of all tests Considered trend of all tests, biased towards nearest Other (specify) 				
5	Please explain the reasons for your answer to Q4	Free text	Distances between soundings are rather comparable. What is more, none of the tests is localized in the nearest proximity of the pad footing. Variability of the test results (particularly up to 4 m below ground level) is not considerable. I decided to take into consideration each of the tests, however, sounding CPT4 was treated as a leading test (the lowest distance between centre of foundation and available soundinge)				
		SERVICEABI					
6	Which parameters did you use for	Tick all that	\boxtimes Cone resistance q _c \square Cone sleeve friction f _s				
	the SLS design of the spread foundation?	apply	 ☑ Young's modulus of elasticity E´ □ Poisson's ratio v □ Shear modulus of elasticity G □ Other (specify) 				
7	What correlations did you use to derive soil parameter values (if used) for the SLS verification? If more than one, please list others below	Free text	Description: E' = 2,5 x qc Author: Schmertmann, J.H. Title: Improved strain influence factor diagrams, ASCE Journal of the Geotechnical Engineering Division, Vol. 104, No. 8, August 1978				
7a	Any other correlations? (please give same info as above)	Free text	-				
8	What assumptions did you make in choosing these correlations?	Free text	As far as I know, the equation $(E'=2,5 \times q_c)$ was derived by Schmertmann from in situ load tests and relations between deformation modulus and cone penetration resistance for normally consolidated soils.				
9	How did you account for any variation in parameters with depth?	Tick one	□ Ignored variation with depth □ Assumed linear variation □ Assumed bi-linear variation ⊠ Assumed stepped variation □ Other (specify)				
10	Please explain the reasons for your answer to Q9	Free text	The method used in settlement calculations requires dividing of soil mass on a finite number of layers. Each layer represents a soil stiffness consistent with test results (in this case q_c). As long as q_c value is not constant with depth, automatically stepped variation is taken into account.				
11	What is the characteristic value of q_c at these depths?	Provide values in units of MPa	At 1 m, $q_c = 11,70$ At 2 m, $q_c = 14,85$ At 4 m, $q_c = 15,38$				
12	What is the characteristic value of E´for a linear elastic calculation at these depths?	Provide values in units of MPa	At 1 m, E ['] = 29,25 At 2 m, E ['] = 37,12 At 4 m, E ['] = 38,45				
13	How did you assess these values?	Tick all that apply	 By eye By linear regression By statistical analysis From an existing standard (specify) From a published correlation (specify) Comparison with a previous design From the soil description, not using the data Other (specify) 				
14	Which calculation model did vou	Tick one	□ Annex F.1 from EN 1997-1 □ Annex F.2 from EN 1997-1				

	use to determine settlement?		☑ Annex D.3 from EN 1997-2 □ Annex D.4 from EN 1997-2				
			LI Annex D.5 from EN 1997-2				
			Alternative from national standard (specify)				
			☐ Finite element analysis ☐ Finite difference analysis				
15	What width does the foundation	Provide	□ Other (specify)				
15	need to avoid a serviceability limit	value in m	DSLS = 2,0				
	state?						
ULTIMATE LIMIT STATE							
10	the ULS design of the spread	apply	⊠ Angle of shearing resistance ϕ □ Effective cohesion c				
	foundation?		\Box Angle of interface friction δ				
17	What correlations did you use to	Eroo toxt	\Box Other (specify)				
17	derive soil parameter values (if	FIEE LEXL	Description: $\varphi = 13,5 \times qc + 23$				
	used) for the ULS verification? If		Author:				
	more than one, please list others below		Title: DIN4094				
170	Any other correlations? (places	Froe text	Pages:				
17a	give same info as above)	FIEE LEXI	-				
18	What assumptions did you make in	Free text	As it is mentioned in annex D.2 the equation which may be used for evaluation of internal friction angle is valid for poorly- graded sands (Cu < 3) above groundwater and cone				ich may be
	choosing these correlations?						
			penetration resistances in the range 5 \leq qc \leq 28 MPa. It was				
			assumed that soil conditions which are presented in the example satisfy requirements which are needed to implement				
			equation from point 17.				
19	What is the characteristic value of	Provide values in	At 1 m, φ´ =37,	4 At 2 m, φ	´ = 38,8	At 4	- m, φ´ = 39.0
	φ at these depths?	degrees					
20	Which calculation model did you	Tick one	⊠ Annex D from EN 1997-1				
	use to determine bearing resistance?		 □ Alternative given in a national annex (specify) □ Alternative given in a national standard (specify) □ Terzaghi □ Meyerhof □ Brinch-Hansen 				
			□ Finite element analysis □ Finite difference analysis				
21	Which country's National Annex did	Free text	Polish standard PN-81/B-03020 Foundation bases. Static				
	you use to interpret EN 1997-1?	Tiele and	computations and design.				
22	use for verification of the Ultimate	lick one	Design Approach 1 Combinations 1 and 2				
	Limit State (ULS)?		□ Design Approach 1 Combination 2 only □ Design Approach 2 □ Design Approach 2* □ Design Approach 2				
			□ Design Approach 3 □ Other (specify)				
23	What values of partial factors did	Provide	1 st combination 2 nd combination (if u		n (if used)		
23a	you use for this ULS verification?	values	γ _G = 1,35	γ _Q = 1,5	γg		γα
			$\gamma_{\phi} = 1$	γc= 1	γ_{ϕ}		γς
			γRv	$\gamma_{Rd} = 1,4$	γRv		γRd
24	What width does the foundation	Provide	Buls = 1,4				
	need to avoid an ultimate limit state?	value in m					
25	What are the structural forces (at its	Provide	Design bending moment M_{Ed} Design shear force V_{Ed} =			orce V _{Ed} =	
	centre-line) that the foundation	kNm and kN	= 0 2453				
	Eurocode 2?						
CONCLUDING QUESTIONS							
26	What other assumptions did you	Free text					
	design?						
27	Please specify any other data that	Free text	Additionally, flat dilatometer tests are desirable to obtain more				
	you would have liked to have had to		reliable soil stiffness parameters (serviceability limit state).				
			capacity of shallow foundations in cohesionless soils (e.g.				

28	How conservative do you consider	Tick one	Annex D.4 from EN 1997-1), then from my point of view cone penetration tests results are adequate enough to obtain angle of internal friction.				
	be for this design example?		· · · · · · · · · · · · · · · · · · ·				
29	How conservative do you consider Eurocode 7 (with your National Annex) to be for this example?	Tick one	 □ Very conservative □ Conservative ⊠ About right □ Unconservative □ Very unconservative 				
30	How does your Eurocode 7 design compare with your previous national practice?	Tick one	 Much more conservative More conservative About the same I Less conservative Much less conservative 				
31	Please provide any other relevant information needed to understand your solution to this design exercise	Free text					
PLEASE SUBMIT YOUR ANSWERS AT <u>www.eurocode7.com/etc10/Example 2.1</u> THANK YOU FOR YOUR CONTRIBUTION!							